

# D1 Servo Drive







# **HIWIN INDUSTRIE 4.0 Best Partner**



#### Linear Motor Stage

- Semiconductor / Precision / Automated Transport /
- Automated Optical Inspection (AOI)
- Planar Servo Motor • Air Bearing Platform

Direct Drive Motor Machine Tools / Semiconductor / Lithium-ion Battery / Laser Marking / Wafer Dicing • Torque Motor-- TM-2 / IM-2, TMRW Series

- X-Y Stage
- Gantry Systems
- Single-Axis Linear Motor Stage



#### Linear Motor

Machine Tool / Semiconductor / Touch Panel / Laser Manufacturing Machine / Glass Cutting Machine

- Iron Core Linear Motor--LMSA,
- LMSA-Z, LMFA, LMFC, LMFP Series • Ironless Linear Motor--LMC Series
- Tubular Motor--LMT Series

Torque Motor &



### 

#### Controller / Drive / AC Servo Motor

PCB / Display / Machine Tools / Semiconductor / Automated / Food / Automated Optical Inspection (AOI)

- Industry Controller--HIMC
- Drive--E1, E2, D1, D2T Series • AC Servo Motor--
- E1 Series, FR Series, abi Series

#### Position Measurement System

PCB / Woodworking / Automation / Warehouse Automation Programmable Industry

- High Resolution--PM-A, PM-B, PM-C
- Signal Translator
- High Performance Counter

#### Multi-Axis Robot

Pick-and-Place / Assembly / Array and Packaging / Semiconductor / Electro-Optical Industry / Automotive Industry / Food Industry

- Articulated Robot • SCARA Robot
- Electric Gripper
- Integrated Electric Gripper

#### Torque Motor

#### Rotary Table

Medical / Automotive Industry / Machine Tools / Machinery Industry

- RAB Series
- RAS Series
- RCV Series
- RCH Series

#### Linear Guideway

Automation / Semiconductor / Medical

- Ball Type--HG, EG, WE, MG, CG
- Quiet Type--QH, QE, QW, QR
- Other--RG, E2, PG, SE, RC

#### Single-Axis Robot

Precision / Semiconductor / Medical / FPD

- KK, SK • KS, KA
- KU, KE, KC





- Precision Ground / Rolled
- Super S Series
- Super T Series
- Mini Roller
- Ecological & Economical Lubrication Module E2
- Rotating Nut (R1)
- Energy-Saving & Thermal-Controlling
- (Cool Type) Heavy Load Series (RD)
- Ball Spline



- 
- 







#### Linear Actuator / Servo Actuator

Medical / Automation / Electric Servo Press / Barrier-free Equipment Industry • Servo Actuator--LAA Series

DMS, DMY, DMN, DMT Series

• Linear Actuator--LAM, LAS, LAN, LAC Series

#### Semiconductor Subsystem



- (Equipment Front End Module)
- Wafer Robot
- 
- EFEM
- 
- 
- 
- Load Port
- Wafer Aligner

# Contents D1 Series Drive



## 1. Features

### ■ Excellent Performance

The D1 drive attains high positioning performance to compliment the motion control technology of the semiconductor industry. The D1 drive achieves very good following characteristics and effectively shortens the positioning time.

### ■ Simple Operation

Human-machine interface provides very simple settings. All standard types of motors and encoders are built inside. Setup can be completed with just one-click.

### ■ Complete Tool Sets

There are test interfaces for speed and acceleration protection settings, gain settings, and an I/O test. Plus the D1 drive has a complete filter, frequency analysis, Bode plot, Lissajous figures and other functions which provide a complete drive control program.

### ■ Easy Integration

HIWIN provides positioning modules, motors, and the best servo drive solution from mega-fabs. According to customer's requirements we can integrate all that are required for user's easiness of application.

### ■ Services

Through HIWIN's complete global presence, we can provide immediate technical services at any time.

### ■ EtherCAT

The D1 series delivers the high performance amplifier with EtherCAT interface



# 2. Application international Safety Standard



### 3. Order Code



### 4. Overall Wiring



### mega-fabs D1 Servo Drive

- Digital amplifier
- Field oriented control
- Intuitive Lightening interface
- 100-240VAC input power
- Supports Step/Direction, CW/CCW and A/B phase pulse format
- Supports analog and digital encoder



- ① Motor Cable
- ② Encoder Cable
- ③ RS-232 Cable
- ④ Regenerative Resistor
- ⑤ Controller Pulse Cable

### 4.1 Wiring Diagram

■ Single-phase power (Brake without relay, using HIWIN motor)





### ■ Three-phase power (Brake without relay, using HIWIN motor)

### 4.2 Control Circuit

#### ■ Wiring Example of Position Control Mode

- Linear Motor Stage



#### Descriptpion:

Wiring example of Position Mode with liner motor. Pulse command input is differential signal.

- Direct Drive Motor



Descriptpion: Wiring example of Position Mode with liner motor. Pulse command input is differential signal.

- Velocity/Torque



Descriptpion:

Wiring example of Velocity/Torque Mode with liner motor.

## 5. Drives

### 5.1 Basic Specifications







Note \* - Only for non EtherCAT drive

### 5.2 Dimensions of drive

### ■ (D1-xx-xx-x-0-xx)







■ (D1-xx-xx-x-2-xx)



# 6. Accessories

### 6.1 Motor Power Cable



#### □□ Represents cable length as the following:



### 6.2 Feedback Signal Cables



#### □□ Represents cable length as the following:



### 6.3 Control Signal Cables



Cable length(m) 3 4 5 6 7 8 9 10

### 6.4 RS232 Communication Cable



### 6.5 Accessory Pack of Connector



### 6.6 EMC Accessory Pack



■ Single phase filter (D1-EMC1)





■ Three phase filter (D1-EMC2)





■ Edge filter (MF-40-S)







■ Three phase filter (D1-EMC3)









#### ■ EMI core



### 6.7 Other Accessories



### ■ Regenerative resistor













### 7. Motor Line-up

### ■ Motor Line-up

#### ■ D1-XX-X2 or D1-XX-X3 for Linear motors

#### LMC :

LMC-EFC1, LMC-EFC2, LMC-EFC3, LMC-EFC4, LMC-EFE6, LMCA2, LMCA3, LMCA4, LMCA5, LMCA6, LMCB2, LMCB3, LMCB4, LMCB5, LMCB6, LMCB7, LMCB8, LMCBA, LMCC7, LMCC8, LMCD4, LMCD6, LMCD8, LMCDA, LMCE4, LMCE6, LMCE8, LMCEA, LMCEC, LMCF4, LMCF6

LMS :

LMSC7, LMSC7(WC)

#### LMFA :

LMFA0x, LMFA1x, LMFA2x, LMFA3x, LMFA4x, LMFA5x, LMFA6x

LMSA :

LMSA1x, LMSA2x, LMSA3x, LMSACx

#### LMT :

LMT2D, LMT2Q, LMT2T, LMTA2, LMTA3, LMTA4, LMTB2, LMTB3, LMTB4, LMTC2, LMTC3, LMTC4, LMTD2, LMTD3, LMTD4

#### ■ D1-XX-X2 for Torque motors

TMS : TMS0x, TMS1x, TMS3x, TMS7x TMN : TMNxxE

#### ■ D1-XX-X4 for Absolute Resolver Torque motors

TMY : TMY4x, TMY6x, TMYAx TMN: TMNxxA



# 8. Selecting motor capacity guide

### 8.1 Motor Sizing

### ■ Start Motor Sizing

The following contents describe how to choose proper motor according to speed, moving distance, and loading inertia. The basic process for sizing a motor is:

- Decide motion profile and required parameters
- Calculate peak and continuous force
- Select motor

#### ■ Symbols

- X : move distance (mm)
- T : move time (sec)
- a : acceleration (mm/s<sup>2</sup>)
- V : velocity (mm/s)
- $M_1$ : loading (kg)
- $g :$  gravitation acceleration (mm/s<sup>2</sup>)
- Fp : peak force (N)
- $F_c$ : continuous force (N)
- Fa : attraction force between stator and forcer (applicable for LMS, LMF series) (N)
- Fi : inertia force (N)
- Kp : force constant (N/Arms)
- I<sub>p</sub> : peak current (Arms)
- I<sub>e</sub> : effective current (Arms)
- I<sub>C</sub>: continuous current (Arms)
- $V_0$ : starting velocity (mm/s)

#### ■ STEP 1 Decide motion velocity profile and required parameters

In order to determine the correct motor for a particular application it is necessary to be familiar with the motion equation.

#### ■ Motion equation

Basic kinematics equations are described as follows:

$$
V = V_0 + aT
$$
  

$$
X = V_0T + \frac{1}{2}aT^2
$$

Where V is velocity, a is acceleration, T is move time and X is move distance.

You can choose two of the four parameters (V, a, T and X) as your designed parameters, then the last two .<br>narameters can be calculated by above equations Parameters can be calculated by above equations.

#### ■ Motion velocity profile

#### 1. 1/3-1/3-1/3 trapezoid profile

If the distance (X) and move time (T) have been given, the most common and efficient velocity profile for point-to-point motion is the "1/3-1/3-1/3" trapezoid curve because it provides the optimal move by minimizing the power required to complete the move. It breaks the time of the acceleration, traveling, and deceleration into three segments as shown below.



 Herein the parameters are described as motion equation. 2  $n<sub>2</sub>$ max Herein the parameter:

#### 2. 1/2-1/2 triangle profile

If X and T are given, another common motion profile is the 1/2-1/2 triangle profile. The motion is divided into two parts, namely acceleration and deceleration. The second motion velocity profile is shown as follows.



The acceleration required in the first motion velocity profile is bigger than that in the second motion velo-4X city profile; therefore, the required motor size is bigger. When choosing second motion velocity profile, the chy pronte; therefore, the required motor size is bigger. When choosing second motion velocity pronte, tr<br>chosen motor size is smaller, however, we need to verify the DC bus of drive is bigger enough, due to the higher velocity (V<sub>max</sub>).

#### 3. Some useful equations



### ■ STEP 2 Determine peak force and effective force

The peak force can be calculated by the follow equation 2 The peak force can be calculated by the follow equation

 $F_p = M_L \times a_{max} + (M_L \times g + F_a) \times \mu = F_i + F_f$ 

Where F<sub>i</sub> is inertia force while F<sub>f</sub> is friction force, and μ is friction factor.

In most cases, motions are cyclic point-to-point movements. Assuming a cyclic motion shown in the following profile with a pause time of t $_4$  second, the effective force can be calculated as following formula:<br> ollowing profile with a pause time of  $t_4$  second, th



The peak current  $I_p$  and effective current  $I_e$  can be calculated by using motor force constant  $K_f$ .  $\mathcal{O}$ The peak current i<sub>p</sub> and

$$
I_p = \frac{F_p}{K_f}
$$
  

$$
I_e = \frac{F_e}{K_f}
$$

#### $\blacksquare$  STEP 3 Select motor by peak force and verify the current supply of motor  $\mathcal{L}_{\mathcal{A}}$ TEP 3 Select motor by peak force and verify the current <mark>s</mark>

 $-$  5 Ferrest Constant on the specification of the setting the start city supply of motor.<br>From the catalog of HIWIN, you can check the specifications of motor and choose an applicable motor by peak force, and then you can verify the current supply if it is fitted the specification as follows.

$$
I_p = \frac{F_p}{K_f} < I_p \text{ (from specification of chosen motor)}
$$
\n
$$
I_e = \frac{F_e}{K_f} < I_c \text{ (from specification of chosen motor)}
$$

Regarding effective and continuous current, the ratio of l<sub>e</sub>/l<sub>c</sub> had better be less than 0.7 to attain some margin. .<br>Ing effective and continuous current, the ratio

#### ■ Linear motor sizing example<br>Ferensels if lad is Flut (parties are 1.875 (m/sec) 0.4 T inear motor sizing example<br>systemle if lood is 5 kg (maxing moos of mos

 $\overline{a}$ 

F

For example, if load is 5 kg (moving mass of mechanism is 1 kg and payload is 4 kg), friction factor μ is 0.01 , distance is 500 mm, move time is 400 ms and dwell time is 350 ms.

, abtaince is ocommit, more time is 400 mis and a well time is 600 mis.<br>At first, we can calculate the V<sub>max</sub>, a<sub>max</sub>, F<sub>p</sub> and F<sub>e</sub> by the formulas described above (choose the first motion velocity profile and LMC series) [ ] 2 2 2 e I <sup>F</sup> <sup>I</sup> = < (from specification of chosen motor)

$$
V_{max} = 1.5 \times \frac{X}{T} = 1.5 \times \frac{0.5}{0.4} = 1.875 \text{ (m/sec)}
$$
  
\n
$$
a_{max} = \frac{4.5 \times X}{T^2} = \frac{4.5 \times 0.5}{(0.4)^2} = 14.06 \text{ (m/sec}^2)
$$
  
\n
$$
F_p = M_L \times a_{max} + (M_L \times g + F_a) \times \mu
$$
  
\n
$$
= 5 \times 14.06 + 5 \times 9.81 \times 0.01 = 70.3 + 0.49 = 70.79 \text{ (N)}
$$
  
\n
$$
F_e = \sqrt{\frac{[(70.3 + 0.49)^2 + 0.49^2 + (70.3 - 0.49)^2] \times 0.1333}{0.4 + 0.35}}
$$
  
\n
$$
= 41.92 \text{ (N)}
$$

In this case, we can choose motor of type LMCA6 (p.48) which can provide up to 187(N )of peak force and continuous force 62(N), and the force constant is 33.8 N/A(rms). Then the current supply of motor can be determined as follows f 41.92

$$
I_p = \frac{F_p}{K_f} = \frac{70.79}{33.8} = 2.09 \, (\text{Arms}) < 5.4 \, (\text{Arms})
$$
\n
$$
I_p = \frac{F_e}{K_f} = \frac{41.92}{33.8} = 1.24 \, (\text{Arms}) < 1.8 \, (\text{Arms})
$$
\n
$$
\frac{I_e}{I_c} = \frac{1.24}{1.8} \times 100\% = 68.89\% < 70\%
$$

### 8.2 Sizing a Regenerative Resistor

# ■ Gather required information<br>■ Gather required information

To calculate the power and resistance of the regen resistor requires information about the amplifier and the motor. For all applications, gather the following information:<br>

- Detail of motion profile, including acceleration and velocity
- Amplifier model number
- Applied line voltage to amplifier<br>————————————————————
- Applied the voltage to amplifier<br>Foque/force constant of the motor
	- -<br>- Resistance (line-to-line) of the motor windings

For rotary motor applications, gather additional information<br>Lead in suit assess by the mater. <sup>3</sup> <sup>P</sup>

- Load inertia seen by the motor f
- Inertia of the motor  $\overline{2}$  firef that of the motor

For linear motor applications, gather additional information E E E 172 48 124 (joule)  $\mathbf{u} = \mathbf{u}$ −or mear motor applica

- Moving mass 1 W W

### $\blacksquare$  Observe the properties of each deceleration during a complete cycle of operation  $\mathcal{L}$  (V  $\mathcal{L}$  )  $\mathcal{L}$  (V  $\mathcal{L}$

For each deceleration during the motion cycle, determine:

- Speed at the start of the deceleration
- Speed at the start of the deceleratio<br>- Speed at the end of the deceleration
- Time over which the deceleration takes place

### $\blacksquare$  Calculate energy returned for each deceleration

The energy returned during each deceleration can be calculated by the following formulas. 2 who end gy recented defined<br>Rotary motor:

 $E_{\text{dec}} = \frac{1}{2} J_{\text{t}} (\omega_1^2 - \omega_2^2)$ 

Edec (joules): Energy returned by the deceleration  $J_t$  (kg m<sup>2</sup>): Load inertia on the motor shaft plus the motor inertia<br> $\Omega$  frediens (see). Shoft aneed at the start of deseleration  $\omega_{\textrm{\tiny{1}}}$  (radians /sec): Shaft speed at the start of deceleration  $\omega$   $_{2}$  (radians /sec): Shaft speed at the end of deceleration l<sub>e</sub> : effective current (Arms)

Linear motor:

 $\overline{a}$ 

$$
E_{\text{dec}} = \frac{1}{2} M_{\text{t}} (V_1^2 - V_2^2)
$$

 $\mathsf{E}_{\mathsf{dec}}$  (joules): Energy returned by the deceleration

Mt (kg): Moving mass 2 <sup>3</sup> <sup>P</sup> <sup>=</sup> אין נגט): שטעוויט ווופא<br>V<sub>1</sub> (meters /sec): Velocity at the start of deceleration

V<sub>2</sub> (meters /sec): Velocity at the end of deceleration

### ■ Determine the amount of energy dissipated by the motor <sup>86</sup> <sup>2</sup> <sup>172</sup>(joule) <sup>2</sup>

■ Determine the amount of energy dissipated by the motor<br>Calculate the amount of energy dissipated by the motor due to current flow through the motor winding resistance using the following formula.

$$
P_{\text{motor}} = \frac{3}{4} R_{\text{winding}} (\frac{F}{K_{\text{t}}})^2
$$

P<sub>power</sub> (watts): Power dissipated in the motor  $P_{\text{power}}$  (watts): Power dissipated in

Rwinding (ohm): Line to Line resistance of the motor coil

- F : Force need to decelerate the motor
	- Nm for rotary applications N for linear applications
- $K_t$ : Torque constant for the motor Nm/Amp for rotary applications N/Amp for linear applications

Emotor = Pmotor Tdecel Emotor (joules): Energy dissipated in the motor T<sub>decel</sub> (seconds): Time of deceleration

#### ■ Determine the amount of energy returned to the amplifier

Calculate the amount of energy that will be returned to the amplifier for each deceleration using the following formula

Ereturned = Edec-Emotor

Leturned Used motor<br>E<sub>returned</sub> (joules): Energy returned to the amplifier

Edec (joules): Energy returned by the deceleration

<sup>M</sup> (<sup>V</sup> <sup>V</sup> ) <sup>2</sup>  $\mathsf{E}_{\mathsf{motor}}$  (joules): Energy dissipated by the motor  $\frac{1}{\sqrt{2}}$   $\frac{1}{\sqrt{2}}$ 

#### ■ Determine if energy returned exceeds amplifier capacity

Compare the amount of energy returned to the amplifier in each deceleration with the amplifier's Compare the amount of energy returned to the amplifier in each deceleration with the amplifier's<br>absorption capacity. The following formula is used to determine the energy that can be absorbed by the amplifier.

$$
W_{\text{capacity}} = \frac{1}{2} C (V_{\text{regen}}^2 - (1.414 V_{\text{mains}})^2)
$$

V<sub>mains</sub>(volts): Mains voltage (AC) applied to the amplifier<br> V<sub>regen</sub>(volts): Voltage at which the regen circuit turns on W<sub>capacity</sub> (joules): The energy that can be absorbed by the bus capacitor C (farads): Bus capacitance

### ■ Calculated energy to be dissipated for each deceleration

calculate the energy that must be dissipated by the regen resistor.<br> $\mathsf F$ For each deceleration where the energy exceeds the amplifier's capacity, using the following formula to

en<br>E<sub>regen</sub> = E<sub>returned</sub> — E<sub>amp</sub>

 $\mathsf{E_{regen}}$  (joules): Energy that must be dissipated in the regen resistor

 $\mathsf{E}_{\sf returned}$  (joules): Energy delivered back to the amplifier from the motor

1 E<sub>returned</sub> youtes): Energy delivered back to the ampli<br>E<sub>amp</sub> (joules): Energy that the amplifier will absorb

#### alculate p <sup>1880</sup> <sup>10</sup> (<sup>390</sup> (1.414 <sup>220</sup>) ) <sup>2</sup>  $\blacksquare$  Calculate pulse power of each deceleration that exceeds amplifier capacity

E W returned capacity > calculate the pulse power that will be dissipated by the regen resistor For each deceleration where energy must be dissipated by the regen resistor, use the following formula to

 $P_{pulse} = E_{regen} / T_{decel}$ 

P<sub>pulse</sub> (watts): Pulse power

 $E_{\text{regen}}$  (joules): Energy that must be dissipated in the regen resistor

T<sub>decel</sub> (seconds): Time of de = Legen ( ) = 2002 / 2009 3 max masses to an

#### ■ Calculate resistance needed to dissipate the pulse power

regen resistor required to dissipate the maximum pulse power. Using the maximum pulse power from the previous calculation, calculate the resistance value of the

regen resistor required<br>R = V<sup>2</sup>regen / P<sub>pulse max</sub>



R(ohms):Resistance

Ppulse max:The maximum pulse power V<sub>regen</sub> :The voltage at which the regen circuit turns on Choose a standard value of resistance less than the calculated value. The value must also be greater than the minimum regen resistor value specified by the amplifier supplier.

#### ■ Regenerative resistor sizing example

Gather required information LM ROBOTS type: LMXL1L-S37L-1200-G200 Amplifier: mega-fabs D1 n<br>DC bus capacitance: 1880uF Regen circuit turn on voltage: 390V Minimum resistance: 15Ω Moving mass: 86Kg (include payload 74 Kg) <sup>M</sup> (<sup>V</sup> <sup>V</sup> ) <sup>2</sup> <sup>1</sup> <sup>E</sup> <sup>2</sup> 2 2 dec = <sup>t</sup> <sup>1</sup> −  $V_{\text{max}}$ : 2 m/s Acceleration, deceleration: 5 m/s2 Acceter ation, deceter ation: 5 m/s-<br>Power supply (AC) of drive: 220VAC Motor type: LMS37L Force constant (Kf): 68N/A(rms) r orce constant (Kr), oorlyArms)<br>R<sub>winding</sub>: 2 ohms(line-to-line)

Calculate regen resistor as following step:

$$
F = ma = 86 \times 5 = 430 (N)
$$
  
\n
$$
E_{dec} = \frac{1}{2} m_t V^2 = \frac{1}{2} \times 86 \times 2^2 = 172 \text{(joule)}
$$
  
\n
$$
P_{motor} = \frac{3}{4} \times R_{winding} \times (\frac{F}{K_t} \times \sqrt{2})^2 = \frac{3}{4} \times 2 \times (\frac{430}{68} \times \sqrt{2})^2
$$
  
\n
$$
= 120 (Watt)
$$
  
\n
$$
E_{motor} = P_{motor} \times T_{decel} = 120 \times (\frac{2}{5}) = 48 \text{ (joule)}
$$
  
\n
$$
E_{returned} = E_{dec} - E_{motor} = 172 - 48 = 124 \text{ (joule)}
$$
  
\n
$$
W_{capacity} = \frac{1}{2} \times C \times (V_{regen}^2 - (1.414V_{mains})^2)
$$
  
\n
$$
= \frac{1}{2} \times 1880 \times 10^{-6} \times (390^2 - (1.414 \times 220)^2)
$$
  
\n
$$
= 51.98 \text{ (joule)}
$$
  
\n
$$
\therefore E_{returned} > W_{capacity}
$$
  
\n
$$
E_{regen} = E_{returned} - E_{amp} = 124 - 51.98 = 72.02 \text{(joule)}
$$
  
\n
$$
P = F_{Garn} = \frac{17}{2} \times 120 \text{ (joule)}
$$

$$
P_{\text{pulse}} = E_{\text{regen}} / T_{\text{decel}} = 72.02 / 0.4 = 180.05 \text{(Watt)}
$$
\n
$$
R = \frac{V_{\text{regen}}^2}{P_{\text{pulse}}} = \frac{390^2}{180.05} = 844.77 \text{(ohms)}
$$

Because the total value of selected resistance must be less than 844.77 ohms and the power capacity must be more than 180.05 watts, we choose two resistors and connect them in series, in each resistor the resistance is 68 ohms and power capacity is 100W. The total resistance value is 136 ohms and power capacity is 200W. The resistance order number is 050100700001. ω<sup>1</sup>  $rac{1}{2}$ 

### 9. Linear Motor Requirements List

Date :



Manager : Salesperson : Salesperson : Salesperson : Salesperson : Salesperson :





### D1 Servo Drive Technical Information

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